

COMPUTATIONAL TECHNOLOGY FOR COMPARISON
OF TWO METHODOLOGIES FOR POSITION
FINDING SEARCH REGIONS

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THESIS

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OF TWO METHODOLOGIES FOR POSITION
FINDING SEARCH REGIONS

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Computational Technology for Comparison
of
Two Methodologies for Position Finding Search Regions

by

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ABSTRACT

This thesis considers two models for the computation of position finding confidence, one of which utilizes a bivariate normal distribution of region, and the other a chi-square distribution. The two models are based on different assumptions, these are explained and explored. A computer simulation model is presented which utilizes both position finding models under varying conditions.

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I. INTRODUCTION

Bearings are taken on an emitter (target) of unknown geographic location by n stations of known location. The best point estimate (BPE) of the target is then calculated, along with a confidence, or search, region within which the target may be said to be located with a given probability. This constitutes the classic radio direction finding position location problem.

This classic problem is part of a general class of position estimation problems whose basic approach is identical, which is the calculation of a point location from a number of lines of position.

Variant problems in this class occur when lines of position are established from ranges, or relative times of arrival of an emission, or when the object to be located takes the measurements on the reference stations.

While this paper examines the classic problem, much of the methodology applies to this more general class of problems.

The BPE is the primary result of a position location solution. The confidence region amplifies this information in two ways. The size of the confidence region serves as a measure of the reliability of the BPE, a larger region implying a more tenuous location. The region also describes an area in which the target will be located with specified confidence. The geometric details of this region provide the more likely locations for search.

II. COMPUTATION OF CONFIDENCE REGIONS

A typical [6] sequence of operations for a position estimation by computer is as follows: A first point estimate is made and a plane surface tangent to the earth is established at that point. Remaining computations are made in the plane rather than the surface of the earth. Unusable, or wild, bearings are rejected and a BPE made utilizing the remaining bearings. A confidence region is computed using the same bearings.

More than one mathematical method is available for most of the steps [3, 4, 8, 9, 11]. The two methods used herein for confidence region computation are designated the bivariate normal (BVN) and the chi-square (χ^2).

The Bivariate normal region [3, 4] is the most commonly used. This region is the family of concentric ellipses

$$ax^2 - 2bxy + cy^2 = -2 \log (1 - P)$$

where P = probability that the target is found within the ellipse

x, y = coordinates in local (to the target) reference system

$$a = \sum_{j=1}^n \frac{\cos^2 \theta_j}{\sigma_j^2}$$
$$b = \sum_{j=1}^n \frac{\sin \theta_j \cos \theta_j}{\sigma_j^2}$$
$$c = \sum_{j=1}^n \frac{\sin^2 \theta_j}{\sigma_j^2}$$

θ_j = bearing observed by station j
 σ_j^2 = variance of displacement of j^{th} line of bearing
 n = number of bearings

The bearings from the stations are assumed to be normally distributed with a mean of zero, and are displaced parallel to the true bearing at the site of the BPE. The confidence region lies in a plane tangent to the surface of the earth at the BPE as calculated by the least squares method [3, 4].

The BVN confidence region requires several assumptions:

- (1) The position lines are great circles on the surface of the earth.
- (2) Measurement error is Gaussian with mean zero.
- (3) Displacement of position lines from the true position line is parallel to the true position line.
- (4) The earth is flat in the vicinity of the confidence region.

These last two assumptions represent approximations that are made to simplify the calculation of the confidence region. Thus, the calculated region is an approximation. The parallel bearing displacement is an approximation of the actual displacement of a point on the bearing by a bearing error. From this, the probability distribution of the points is developed [4]. Placing the resultant curves in a plane adds an additional distortion, which grows with the size of the confidence region [7].

The chi-square confidence region [3, 10] is the family of concentric curves

$$x^2 = \sum_{j=1}^n \frac{1}{s_j^2} \cdot (\theta_j - \beta_j)^2$$

where

s_j^2 = bearing variance of station j

θ_j = bearing observed by station j

β_j = true bearing from station j to a point
(x,y) in the curve

n = number of bearings

x^2 has a chi square distribution with n degrees of freedom. Of the above listed assumptions required by the BVN method, only (1) and (2) are required for the χ^2 region. The region lies on the surface of the earth centered at the minimum x^2 point, rather than in a plane.

Both methods require the estimated variance of the bearings to be used in the calculation. The effect of an incorrect estimation could be much larger than the errors of approximation. Estimates in practice are a function of a stations past performance plus the direction finder operator's evaluation of the reliability of each bearing he observes and reports.

The assumption of Gaussian bearing distribution eliminates the case of wild, or outlying bearings which occur in practice, largely through operator error. As a Gaussian distribution

is basic to both the BVN and χ^2 methods, elimination of wild bearings from the computation is necessary, though the theory of each method would be affected by their assumed existence. Wild bearing rejection methods are available [6, 7]. The use of such methods is usually limited to four or more bearing situations. With two bearings, no basis for detection of wild bearings exists. For most three bearing situations, when the existence of at least one wild bearing is indicated, it is impossible to identify it, or them. With four bearings, one wild bearing can be seen to miss the BPE area formed by the other three.

In practice [6, 7] the Outlier detection and rejection method is used, but a Gaussian distribution is still assumed for those remaining.

Daniels and Vajda [3] object to the use of χ^2 regions on the grounds that it may occur that no points can be found to satisfy the resultant equations.

Read [10] examines the simplifications required in calculating the BVN regions, and compares the two methods. The χ^2 regions are expected to be too small, and the BVN too large, though the full effect of the simplifications by Kukes and Starik [4] is not known.

Comparison of the two methods by computer plotting techniques shows considerable difference in size. Additionally, the effect of the approximations used in the BVN method is apparent. While BVN region is elliptical in all cases, the χ^2 region may assume an egg shape.

A barrier to the use of χ^2 regions is the lack of a way of reporting them. A BVN region can be described by its center, angular orientation, and length of semi axes. No such simplifying parameters exist for χ^2 regions. One possible approach would be to attempt a conversion into a partially equivalent rectangle, square, or circle as is often done for BVN regions [1, 6, 7]. Since these regions are always larger than the computed region, contain areas of lesser probability, and omit areas of greater probability, any advantage of using one method over the other would probably be lost thereby.

A thorough investigation of the two methods is required, in order to determine the actual probabilities represented by each type of confidence region. The differences indicate that at least one of the methods has error. A computer simulation was written to compare them.

III. COMPUTER SIMULATION MODEL

The appended computer program provides a means for simulation of the two confidence region methods for identical input data.

Inputs to the program are station latitude, longitude, and standard deviation of bearing distribution; target latitude and longitude.

The true bearings and distance for each station and target are computed and a bearing error generated and added. This portion contains parts of the Bergh program in Pope [8] and is a program used by LT Paul Winkler, modified here to include more general positions.

A first-point estimate of the position is made by Pope's [9] vector method, and the final fix by the least squares method of Kukes and Starik [4] in a plane tangent to the earth at the first-point estimate. This portion was used by Lunde [5] but contained errors since corrected.

A bivariate normal confidence region is computed by the method of Kukes and Starik, and orientation angle and length of major and minor semi axes generated. Additionally, output by graphic plot is available.

A χ^2 confidence region is then computed and a graphic plot generated. No parameteric output for the χ^2 region is available, as no method yet exists for describing the shape of the region. This portion was originally written by LT Winkler, and since modified to include more general positions.

The subroutines GAMA, for the normalized incomplete gamma function, and MTRMAP, the graphic plot, are from the library of the W. R. Church Computer Center at the Naval Postgraduate School.

The graphic plots are on a grid measured in degrees of a great circle, resembling a Mercator projection at the equator. Hence, visual distortion of the regions occurs as their location approaches the poles, but the geographical points of the χ^2 regions are correct. The geographical points of the BVN regions are correct, except for the distortion caused by the flat earth assumption.

IV. SUGGESTED SIMULATION PROCEDURE

An undetected error in previous work invalidated all data generated. Time constraints prevented regeneration of the data after correction of the error.

The behavior of the regions generated by the two methods differs with the number of stations in the net, configuration of the net, standard deviation of the error used, and relative location of target with respect to the net. Thus, a general case may not exist. A valid comparison would include sufficient combinations to detect all possible patterns of behavior.

A useful measure of effectiveness for the regions would be the difference in the probability level in each of the two regions occupied by the true position of the target.

The standard deviation used in generating bearing error is also used in computing BPE and confidence regions. A minor modification to the program would permit the examination of the consequences of incorrectly estimating the actual bearing distribution of a station, by computing these with a different standard deviation than that used to generate the error.

The errors generated are from a normal distribution, and include no wild bearing. A means of detection for wild bearings is not included in the program. Such a routine may be added to the program, along with a generation routine for wild bearings.

The modifications above would permit examination of more realistic situations through the use of operational data, along with a model of the actual net which supplied the data.

V. AN ALTERNATE APPROACH

An underlying assumption in the methods discussed is that there is a uniform prior probability for the target location. That is, the mathematical solution of the BPE and confidence regions are inputs to the solution of the operational question of target location. Prior knowledge of probable target location does not affect the solution. This approach is intuitively correct generally.

Operationally, there are two uses of position finding information:

- (1) To determine the location of a target of known or unknown identity;
- (2) To identify a target from a set of known targets by its location.

This second use introduces prior information into the problem, and occurs usually when attempting to identify a fixed land-based station.

Butterly [2] describes a method for incorporation of information of this type in producing a Bayesian position estimate, though he implies that its use could be more general.

A further modification of the program would permit a test of the efficacy of this method by comparing the number of correct identifications when using the Bayesian method with the number when selecting the target in the lowest level of the confidence region. Both the BVN and χ^2 methods could be used in each.

THIS FORTRAN PROGRAM CALCULATES RADIO DIRECTION FINDING POSITION ESTIMATES AND CONFIDENCE REGIONS. SEVERAL OPTIONS IN OUTPUT ARE AVAILABLE, AND ARE DOCUMENTED BY COMMENT CARDS IN THE PROGRAM.

INPUTS TO THE PROGRAM ARE:

- 1 - NUMBER OF DIRECTION FINDING STATIONS (ONE CARD, FORMAT I2)
- 2 - LATITUDE, LONGITUDE, AND STANDARD DEVIATION OF EACH STATION (ONE CARD EACH, FORMAT 3F10.4)
- 3 - NUMBER OF TARGETS (ONE CARD, FORMAT I2)
- 4 - LATITUDE AND LONGITUDE OF EACH TARGET (ONE CARD EACH, FORMAT 2F10.4)
- 5 - SIZE OF GRAPHICAL PLOTS IN DEGREES (ONE CARD, FORMAT F10.4)

LIMITS - STATIONS 8
 TARGETS 8

SIGN CONVENTION: LATITUDES NORTH 0 TO +90.0
 SOUTH 0 TO -90.0
 LONGITUDES EAST 0 TO -180.0
 WEST 0 TO +180.0
 BEARINGS EAST OF NORTH 0 TO +180.0
 WEST OF NORTH 0 TO -180.0

PART ONE - INITIALIZATION AND INPUT

```
DIMENSION BETA(10,10)
DIMENSION STEEST(8,8), GAMMA(8,8)
DIMENSION STALAT(10), STALON(10), STDEV(10), TARLAT(20)
DIMENSION TARLON( 20), THETA( 10,20), DIST( 10,20)
DIMENSION WORM(13,13)
DIMENSION PJ(10), ZETA(10)
DIMENSION B1(8), B2(8)
DIMENSION AE(8), BE(8), CE(8), DE(8), EE(8), FE(8)
DIMENSION Y(13,13)
DIMENSION SDRAD(8)
DIMENSION C(13,13)
REAL*4 T(24)
```

```
RADDEG=.017453293
IX=46721
PI=3.141592
RADIUS=10800.0/PI
EX = 0.0
```

READ STATION POINTS


```

      READ(5,100) NSTA
100  FORMAT(I2)
      DO 2 I=1,NSTA
        2  READ (5,102) STALAT(I), STALCN(I), STDEV(I)
102  FORMAT(3F10.4)

```

READ TARGET POINTS

```

      READ(5,100) NTAR
      DO 1 I=1,NTAR
1  READ(5,102) TARLAT(I), TARLON(I)

```

READ GRAPH SIZE

```
READ(5,102) CGRAPH
```

PART TWO - GENERATION OF BEARINGS AND BEARING VARIANCES

THIS SECTION OF PART TWO COMPUTES BEARING ANGLES AND DISTANCES
USING NAPIER'S ANALOGIES

```
DO 10 I=1,NSTA
DO 10 J=1,NTAR
AA=ABS(STALCN(I)-TARLON(J))
IF(AA.GT.180.0) AA=360.0-AA
GAMMA(I,J)=AA
```

CHECK FOR SAME MERIDIAN CASE

```
IF(AA.GT.0.01) GO TO 105
BB=0.0
IF(STALAT(I).GT.TARLAT(J)) BB=180.0
THETA(I,J)=BB
DIST(I,J)=ABS(STALAT(I)-TARLAT(J))*RADIUS*RADDEG
GO TO 23
```

105 CONTINUE

CC=ABS{AA-180.0)


```

IF(CC.GT.0.001) GO TO 106
DD=0.0
SUMLAT=STALAT(I)+TARLAT(J)
IF(SUMLAT.LT.0.0) DD=180.0
THETA(I,J)=DD
EED=180.0-ABS(SUMLAT)
DIST(I,J)=EED*RADIUS*RADDEG
GO TO 23
106 CONTINUE

```

```

CONTINUE SOLUTION OF TRIANGLE

```

```

WVALUE = GAMMA(I,J)*.5*RADDEG
COT1 = COS(WVALUE)/SIN(WVALUE)
BRAVO = 90.0 - TARLAT(J)
ABLE = 90.0 - STALAT(I)

```

```

COS1 = COS((ABLE - BRAVO)*.5*RADDEG)
COS2 = COS((ABLE + BRAVO)*.5*RADDEG)
SIN1 = SIN((ABLE - BRAVO)*.5*RADDEG)
SIN2 = SIN((ABLE + BRAVO)*.5*RADDEG)

```

```

YA=COT1*COS1
YB=COT1*SIN1

```

```

ATA=ATAN2(YA,COS2)
ATB=ATAN2(YB,SIN2)
BBB=(ATA-ATB)/RADDEG

```

```

BBB=ANGLE, NOW COMPUTE PROPER SIGN

```

```

SL=STALON(I)
TL=TARLON(J)
IF(SL.LT.0.0) SL=360.0+SL
IF(TL.LT.0.0) TL=360.0+TL
TL=TL-SL
IF(TL.LT.0.0) TL=TL+360.0
IF(TL.LT.180.0) BBB=-BBB
THETA(I,J)=BBB

```

```

THETA=TRUE BEARING FROM STATION TO TARGET

```

```

DISTANCE FROM STATION TO TARGET USING LAW OF COSINES

```

```

GAMMA(I,J) = GAMMA(I,J)*RADDEG

```



```

TARLAT(J)=TARLAT(J)*RADDEG
STALAT(I)=STALAT(I)*RADDEG
TEMP = SIN(TARLAT(J))*SIN(STALAT(I))+COS(TARLAT(J))*COS(STALAT(I))
1*COS(GAMMA(I,J))
DFDIST = ARCOS(TEMP)
DIST(I,J) = DFDIST*RADIUS

```

DIST=DISTANCE IN NAUTICAL MILES

```

TARLAT(J)=TARLAT(J)/RADDEG
STALAT(I)=STALAT(I)/RADDEG

```

23 CONTINUE

THIS SECTION OF PART TWO ADJUSTS THE STANDARD DEVIATION TO BE USED IN BEARING ERROR COMPUTATION FOR THE DISTANCE BETWEEN STATION AND TARGET. THE SOURCE OF THIS COMPUTATION IS NOT KNOWN.

```

SD = STDEV(I)
R = DIST(I,J)/100.0
IF (R-54.0) 20,20,22
22 SD = SD*(R/(108.0 - R))
GO TO 32
20 IF (R-10.0) 24,26,26
24 IF (R-4.0) 28,30,30
28 SD = PI/2.0
GO TO 32
30 SD = SD*(.0204*R*R - .402*R + 3.0)
GO TO 32
26 SD = SD*(.00071*R*R - .0213*R + 1.1598)
32 STEEST(I,J) = SD*SD*RADDEG*RADDEG
10 CONTINUE

```

```

WRITE(6,253)
253 FORMAT (///,36X,45H BEARING ANGLE FROM ITH STATION TO JTH TARGET,/
1/)
WRITE(6,256)((I,J,THETA(I,J),J=1,NTAR),I=1,NSTA)
256 FORMAT(39X,13HFROM STATION ,I2,
111H TO TARGET ,I2,4H -- ,F10.4)

```

```

WRITE(6,255)
255 FORMAT (//,40X,40HDISTANCES FROM ITH STATION TO JTH TARGET,/)
WRITE(6,256)((I,J,DIST(I,J),J=1,NTAR),I=1,NSTA)

```


C THIS SECTION OF PART TWO COMPUTES BEARING ERROR FROM A SIMULATED
C NORMAL DISTRIBUTION USING A RANDOM NUMBER GENERATOR, AND ADDS THE
C ERROR TO THE TRUE BEARING.

C WRITE(6,260)
C 260 FORMAT (//,50X,15HNORMAL VARIATES,//)

C DO 40 I=1,NSTA
C DO 40 J=1,NTAR
C STEEST(I,J) = STEEST(I,J)/RADDEG
C CALL GASS(IX,STEEST(I,J),EX,X)
C BETA(I,J)=THETA(I,J)+X

C WRITE(6,256)I,J,X

C 40 CONTINUE

C OUTPUT ANGLES WITH ASSOCIATED ERROR

C WRITE(6,200)
C 200 FORMAT (//6X,6HSTALAT, 8X, 6HSTALON, 8X,6HTARLAT, 8X,6HTARLON,
C 18X,10HTHETA(I,J), 4X, 5HSTDDEV)
C WRITE(6,259)((STALAT(I),STALON(I),TARLAT(J),TARLON(J),
C 1 BETA(I,J),STEEST(I,J), J=1,NTAR), I=1,NSTA)
C 259 FORMAT(/,6(F12.5,2X))

C PART THREE - COMPUTATION OF POSITION ESTIMATE, OR FIX

C DO 3321 J1=1,NTAR

C WRITE(6,220) TARLAT(J1), TARLON(J1)
C 220 FORMAT(71H1 THE FOLLOWING BEARINGS WERE TAKEN ON A TARGET LOCA
C 1 TED AT LATITUDE, F12.5,11H LONGITUDE,F12.5,//)
C WRITE(6,300)
C 300 FORMAT(10X,8HLATITUDE,12X,9HLONGITUDE,14X,5HTHETA,11X,12HTRUE BEAR
C 1 ING, 10X, 7HSTD DEV,//)
C WRITE(6,221) (STALAT(I),STALON(I), BETA(I,J1),THETA(I,J1),
C 1 STDDEV(I), I=1,NSTA)
C 221 FORMAT(5(10X,F10.5))

THIS SECTION OF PART THREE CALCULATES A FIRST POINT ESTIMATE OF
THE FIX USING POPE'S VECTOR METHOD (1971)

COMPUTE BEARING PLANE INTERSECTIONS

WRITE(6,701)
701 FORMAT(//,44X,26HBEARING LINE INTERSECTIONS,
1/,40X,8HSTATIONS,4X,8HLATITUDE,4X,
29HLONGITUDE,//)
DO 88 I=1,NSTA

B1(I) = STALAT(I) * RADDEG
B2(I) = STALON(I) * RADDEG

SLAT = SIN(B1(I))
CLAT = COS(B1(I))
SLON = -SIN(B2(I))
CLON = COS(B2(I))
SBNG = SIN(BETA(I,J1)*RADDEG)
CBNG = COS(BETA(I,J1)*RADDEG)

XE = CLAT * CLON
YE = CLAT * SLON
ZE = SLAT

AE(I) = CBNG*SLON - SBNG*SLAT*CLON
BE(I) = -CBNG*CLON - SBNG*SLAT*SLON
CE(I) = SBNG*CLAT

DE(I) = BE(I)*ZE - CE(I)*YE
EE(I) = CE(I)*XE - AE(I)*ZE
FE(I) = AE(I)*YE - BE(I)*XE

88 CONTINUE

USUM = 0.0
VSUM = 0.0
WSUM = 0.0

DO 89 I=2,NSTA
ILIMIT = I-1
DO 90 J=1,ILIMIT

UE = BE(I)*CE(J) - CE(I)*BE(J)
VE = CE(I)*AE(J) - AE(I)*CE(J)
WE = AE(I)*BE(J) - BE(I)*AE(J)


```

TI = UE*DE(I) + VE*EE(I) + WE*FE(I)
TJ = UE*DE(J) + VE*EE(J) + WE*FE(J)

IF (TI*TJ .LT. 0.0) GO TO 90
IF (TI .GT. 0.0) GO TO 91

UE = -UE
VE = -VE
WE = -WE

CCCC
COMPUTE CENTROID OF INTERSECTIONS

91 USUM = USUM + UE
   VSUM = VSUM + VE
   WSUM = WSUM + WE

   UMAG=SQRT(UE*UE+VE*VE+WE*WE)
   ULAT=ARSIN(WE/UMAG)/RADDEG
   ULON=-ATAN2(VE,UE)/RADDEG

   WRITE(6,702)I,J,ULAT,ULON
702  FORMAT(40X,I2,5H AND ,I2,3X,F8.3,4X,F8.3)

   ULAT, ULON = BEARING PLANE INTERSECTIONS

90 CONTINUE
89 CONTINUE

CCCC
CONVERT CENTROID TO LATITUDE AND LONGITUDE OF FIRST POINT ESTIMATE

X1LON = -ATAN2(VSUM,USUM)/RADDEG
X1LAT=ARSIN(WSUM/SQRT(USUM*USUM+VSUM*VSUM+WSUM*WSUM))/RADDEG

WRITE(6,222)
WRITE(6,223) X1LAT, X1LON
222  FORMAT(//,10X,24HTHE FIRST POINT ESTIMATE,/)
223  FORMAT(10X,8HX1LAT = ,F10.5,5X,8HX1LON = ,F10.5,/)

CCCC
THIS SECTION OF PART THREE TRANSFERS THE PROBLEM TO A PLANE TANGENT
TO THE EARTH AT THE FIRST POINT ESTIMATE, THEN COMPUTES A POSITION
ESTIMATE USING THE LEAST SQUARES METHOD OF KUKES AND STARIK.

ASUM=0.0
BSUM=0.0

```



```

CSUM=0.0
DSUM=0.0
ESUM=0.0

```

```

DO 8999 L=1,NSTA
SDRAD(L)=STDEV(L)*RADDEG
CONTINUE
DO 9002 I=1,NSTA
XSI=BETA(I,J1)*RADDEG
XSI=ABS(XSI)

```

```

XSI=STATION BEARING IN RADIAN

```

```

COMPUTE BEARING IN LOCAL REFERENCE PLANE USING NAPIER'S ANALOGIES
AND LAW OF SINES

```

```

RHO=(STALON(I)-X1LON)*RADDEG
RHO=ABS(RHO)
IF(RHO.GT.PI) RHO=(2.0*PI)-RHO

```

```

CHECK FOR DUE NORTH OR SOUTH BEARING

```

```

IF(RHO.GT.0.001) GO TO 345
ZETA(I)=PI
IF(STALAT(I).LT.X1LAT) ZETA(I)=0.0
GO TO 347
CONTINUE
RR=ABS(RHO-PI)
IF(RR.GT.0.001) GO TO 346
ZETA(I)=PI
POLE=STALAT(I)+X1LAT
IF(POLE.LT.0.0) ZETA(I)=0.0
GO TO 347

```

```

346 CONTINUE

```

```

CONTINUE SOLUTION OF TRIANGLE

```

```

CEE=(90.-STALAT(I))*RADDEG
DENOM=.5*(XSI+RHO)
RUM11=.5*(XSI-RHO)
RUM12=.5*CEE

```

```

ANUM=SIN(RUM11)*TAN(RUM12)
DENA=SIN(DENOM)
ARKTN1=ATAN2(ANUM,DENA)
RTA=ABS(DENOM-PI/2)

```



```

RTB=ABS(RUM11-PI/2)
IF(RTA.GT.0.001) GO TO 355
BNUM=COS(RUM11)*TAN(RUM12)
DENB=0.001
GO TO 357
355 IF(RTB.GT.0.001) GO TO 356
BNUM=0.001
DENB=COS(DENOM)
GO TO 357
356 CONTINUE
BNUM=COS(RUM11)*TAN(RUM12)
DENB=COS(DENOM)
357 CONTINUE
ARKTN2=ATAN2(BNUM,DENB)
AAEE=ARKTN1+ARKTN2
IF(XSI.LT.0.001) XSI=0.001
DDD=SIN(CEE)*SIN(XSI)
IF(AAEE.LT.0.001) AAEE=0.001
EEE=SIN(AAEE)
FFF=DDD/EEE
IF(FFF.GE.1.0) FFF=0.999999
CCEE=ARSIN(FFF)

C   ZETA(I)=PI-CCEE
C   IF(AAEE.LT.CEE) ZETA(I)=CCEE
C   IF(BETA(I,J1).LT.0.0) ZETA(I)=-ZETA(I)

347 CONTINUE
ZETA=LOCALIZED BEARING

TAKE NEGATIVE OF ZETA TO CONVERT TO NORMAL TRIG SIGN CONVENTION
ZETA(I)=-ZETA(I)

CALCULATE PERPENDICULAR DISTANCE FROM LOCALIZED BEARING TO
CENTER OF COORDINATE SYSTEM
YPRIM=(90.-XILAT      )*RADDEG
AAEE=ABS(AAEE)
YDIST= (YPRIM-AAEE)
PJ(I)=YDIST*SIN(ZETA(I))

SUM TERMS FOR FOLLOWING CALCULATIONS

```



```

ASUM=ASUM+(COS(ZETA(I))*COS(ZETA(I)))/(SDRAD(I)*SDRAD(I))
BSUM=BSUM+(SIN(ZETA(I))*COS(ZETA(I)))/(SDRAD(I)*SDRAD(I))
CSUM=CSUM+(SIN(ZETA(I))*SIN(ZETA(I)))/(SDRAD(I)*SDRAD(I))

```

9002 CONTINUE

```

DO 9006 K=1,NSTA
DSUM=DSUM+PJ(K)*((BSUM*SIN(ZETA(K))-CSUM*COS(ZETA(K)))/(SDRAD(K)*
1SDRAD(K)))
ESUM=ESUM+PJ(K)*((ASUM*SIN(ZETA(K))-BSUM*COS(ZETA(K)))/(SDRAD(K)*
1SDRAD(K)))

```

9006 CONTINUE

CALCULATE LEAST SQUARES ESTIMATES AND CONVERT TO DEGREES

```

COEF=1.0/((ASUM*CSUM)-(BSUM*BSUM))
XO=COEF*DSUM
YO=COEF*ESUM
SQKO=-2.*ALOG(.1)
XEST=X1LON+XO/RADDEG
YEST=X1LAT+YO/RADDEG

```

XEST, YEEST = LEAST SQUARES ESTIMATE OF POSITION

```

WRITE(6,9007) YEEST,XEST
9007 FORMAT(' ','THE LEAST SQUARES ESTIMATE OF POSITION IS ',F6.2,
1' DEGREES LATITUDE'//43X,F7.2,' DEGREES LONGITUDE'///)

```

PART FOUR - COMPUTATION OF CONFIDENCE REGIONS

THIS SECTION OF PART FOUR CALCULATES A BIVARIATE NORMAL CONFIDENCE REGION (DANIELS, KUKES AND STARIK)

CALCULATE ANGLE BETWEEN MAJOR AXIS OF ELLIPSE AND MERIDIAN

```

AA1=2.*BSUM
AA2=CSUM-ASUM
TWOANG=ATAN2(AA1,AA2)

```



```
IF(BANG)651,651,652
BANG=BANG+(PI/2.0)
GO TO 653
BANG=BANG-(PI/2.0)
CONTINUE
ANG=BANG/RADDEG
```



```

EXVAL=(CGRAPH/2.0)-(((J-1)/12.0)*CGRAPH)
EXVAL=EXVAL*RADDEG
DO 9012 I=1,13
YVAL=(CGRAPH/2.0)-(((I-1)/12.0)*CGRAPH)
YVAL=YVAL*RADDEG
HOO=BSUM*EXVAL*YVAL-(ASUM/2.)*EXVAL*EXVAL-(CSUM/2.0)*YVAL*YVAL
PROB=1.0-EXP(HOO)
WORM(I,J)=PROB

```

```

9012 CONTINUE
9011 CONTINUE

```

```

N=13
M=13
AZ=0.0
BZ=0.0
BND=0.0
AMIN=0.0
IJT=0.0
ICON=1
IGR=1
DO 9080 LL=1,24
9080 T(LL)=0.0

```

```

PRINT THE CONFIDENCE REGION PLOT

```

```

CALL MTRMAP(WORM,N,M,T,BND,AZ,BZ,AMIN,IJT,ICON,IGR)
WRITE(6,591)
591 FORMAT(///,45X,'BIVARIATE NORMAL CONFIDENCE REGION')
WRITE(6,509) CGRAPH,CGRAPH
509 FORMAT(///,20X,37H THE SIZE OF THE CONFIDENCE PLOT IS ,F10.4,
114H DEG. LAT. BY ,F10.4, 12H DEG. LONG. ,/,40X,
241H THE FIX POINT IS LOCATED AT (007, 007). )

```

THIS SECTION OF PART FOUR CALCULATES A CHI-SQUARE CONFIDENCE REGION, AND PRINTS A GRAPHICAL PLOT. NO OTHER OUTPUT IS AVAILABLE. ADDITIONALLY, LEVELS OF CONSTANT VALUE OF Q MAY BE PLOTTED (DANIELS). THIS SECTION MAY BE SKIPPED BY JUMPING FROM THIS POINT TO THE END OF THE MAIN PROGRAM. EITHER THE Q OR CHI-SQUARE PLOTS MAY BE SKIPPED SEPARATELY BY JUMPING AROUND THE APPROPRIATE 'CALL MTRMAP...' CARD AT THE END OF THIS SECTION.

```

X1LAT=YEST
X1LON=XEST
X1LAT = X1LAT + CGRAPH/2.0
X1LON = X1LON + CGRAPH/2.0

```



```

C      DO 501 K = 1,13
      DO 502 L = 1,13
      Y(K,L) = 0.0
C
      DO 571 I=1,NSTA
      G=ABS(STALON(I)-X1LON)
      IF(G.GT.180.0) G=360.0-G
      IF(G.GT.0.001) GO TO 610
      ANGLE=0.0
      IF(STALAT(I).GT.X1LAT) ANGLE=180.0
      GO TO 620
610  CONTINUE
      ABLE=90.0-STALAT(I)
      BRAVO=90.0-X1LAT
      WVALUE=G*.5*RADDEG
      COT1 = COS(WVALUE)/SIN(WVALUE)
      COS1 = COS((ABLE-BRAVO)*.5*RADDEG)
      COS2 = COS((ABLE+BRAVO)*.5*RADDEG)
      SIN1 = SIN((ABLE-BRAVO)*.5*RADDEG)
      SIN2 = SIN((ABLE+BRAVO)*.5*RADDEG)
      RR=COT1*SIN1
      SS=ATAN2(RR,SIN2)
      TT=COT1*COS1
      UU=ATAN2(TT,COS2)
      ANGLE=(UU-SS)/RADDEG
620  CONTINUE
      SL=STALON(I)
      TL=X1LON
      IF(SL.LT.0.0) SL=360.0+SL
      IF(TL.LT.0.0) TL=360.0+TL
      TL=TL-SL
      IF(TL.LT.0.0) TL=TL+360.0
      IF(TL.LT.180.0) ANGLE=-ANGLE
      CHIDIF=ANGLE-BETA(I,J1)
      Y(K,L) = Y(K,L) + CHIDIF*CHIDIF/STDEV(I)/STDEV(I)
      PAR1=NSTA/2.
      PAR2=Y(K,L)/2.
      CALL GAMA (PAR1,PAR2,GAM,B,0.0)
      C(K,L)=1.-GAM
571  CONTINUE
C
502  X1LON = X1LON - CGRAPH/12.0
      X1LON = X1LON + CGRAPH*13.0/12.0
501  X1LAT = X1LAT - CGRAPH/12.0
C
C
C  SET UP THE CONTOUR SUBROUTINE

```



```

C
N=13
M = 13
AZ = 0.0
BZ = 0.0
BND = 0.0
AMIN = 0.0
IJT = 0
ICON = 1
IGR = 1
DO 504 II = 1,24
504 T(II) = 0.0

C
C
C   PLOT THE Q LEVELS
      CALL MTRMAP(Y,N,M,T,BND,AZ,BZ,AMIN,IJT,ICON,IGR)
      WRITE(6,592)
592  FORMAT(///,45X,'LEVELS OF CONSTANT VALUE OF Q')
      WRITE(6,509) CGRAPH,CGRAPH

C
C
C   PLOT THE CHI-SQUARE REGION
      CALL MTRMAP(C,N,M,T,BND,AZ,BZ,AMIN,IJT,ICON,IGR)
      WRITE(6,593)
593  FORMAT(///,45X,'CHI-SQUARE CONFIDENCE REGION')
      WRITE(6,509) CGRAPH,CGRAPH

C
C321 CONTINUE
C
      STOP
      END

      SUBROUTINE GASS(IX,S,AM,V)
      A = 0.0
      DO 50 I=1,12
      CALL WRANDU(IX,IY,Y)
      IX = IY
50  A = A+Y
      V = (A+6.0)*S+AM
      RETURN
      END

```



```
SUBROUTINE WRANDU(IX,IY,Y)
IY = IX*65539
IF (IY) 5,6,6
5 IY = IY + 2147483647+1
6 Y = IY
Y = Y*.4656613E-9
RETURN
END
```


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13. ABSTRACT

This thesis considers two models for the computation of position finding confidence, one of which utilizes a bivariate normal distribution of region, and the other a chi-square distribution. The two models are based on different assumptions, these are explained and explored. A computer simulation model is presented which utilizes both position finding models under varying conditions.

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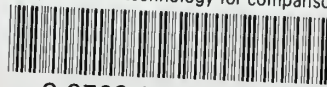
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